## PATENT ABSTRACTS OF JAPAN

(11)Publication number:

2003-120353

(43) Date of publication of application: 23.04.2003

(51)Int.Cl.

F02D 23/00 F02B 37/00 F02B 37/12 F02B 37/18 F02D 21/08 F02D 23/02 F02D 41/04 F02D 41/10 F02D 43/00 F02M 25/07

(21)Application number: 2001-315179

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(22)Date of filing:

12.10.2001

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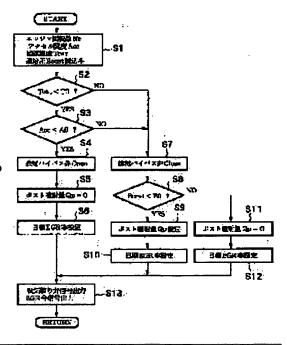
**KAWAMOTO KEIJI** 

# (54) SUPERCHARGING PRESSURE CONTROL DEVICE FOR INTERNAL COMBUSTION ENGINE

#### (57)Abstract:

PROBLEM TO BE SOLVED: To improve the responsiveness of a supercharging pressure rise.

SOLUTION: If the temperature of an exhaust purifying catalyst is low and there is no acceleration request, exhaust bypassing a turbine of a turbosupercharger and maintaining high temperature is led to the catalyst to promote temperature raising activation (Step 1 to 4). In the process, if the catalyst is active or an acceleration request occurs, the exhaust bypassing of the turbine is prohibited, and if supercharging pressure is not higher than a given level, a postinjection is executed to elevate exhaust temperature and promote rises in turbine rotation and interlocked compressor rotation, which in turn suppresses lag in supercharging pressure rise. An excess air ratio corresponding to the postinjection quantity is controlled to suppress degradation in HC, CO and the like (Step 7 to 12).



#### **LEGAL STATUS**

[Date of request for examination]

[Date of sending the examiner's decision of rejection]

[Kind of final disposal of application other than the examiner's decision of rejection or application converted registration]

[Date of final disposal for application]

[Patent number]

[Date of registration]

[Number of appeal against examiner's decision of rejection]

[Date of requesting appeal against examiner's decision of

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rejection] [Date of extinction of right]

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#### **CLAIMS**

[Claim(s)]

[Claim 1] The charge pressure control device of the internal combustion engine which is the charge pressure control device of the internal combustion engine which carried the turbosupercharger which performs inhalation-of-air supercharge by the compressor which rotates with the turbine driven by the exhaust stream, and is characterized by performing postinjection after the Maine injection of a fuel when raising the charge pressure of said turbosupercharger.

[Claim 2] The charge pressure control unit of the internal combustion engine characterized by performing said Maine injection and postinjection with the injector [ ON-OFF / with a solenoid valve / injector / injection of a fuel ].

[Claim 3] The active state of an exhaust air purification means to purify the exhaust air component which is arranged in the flueway of the turbine lower stream of a river of said turbosupercharger, and flows is judged. The bypass flow rate of the exhaust air which bypasses said turbine and is led to said exhaust air purification means when this exhaust air purification means has not carried out activity is enlarged. It is the charge pressure control unit of the internal combustion engine according to claim 1 or 2 characterized by performing said postinjection when switching said bypass flow rate to smallness from size while performing bypass control of flow which makes said bypass flow rate small, when said exhaust air purification means carries out activity.

[Claim 4] The charge pressure control unit of the internal combustion engine according to claim 3 characterized by controlling the opening of the exhaust air bypass valve infixed in the bypass path which bypasses said turbine, and controlling said bypass flow rate. [Claim 5] The charge pressure control unit of the internal combustion engine of any one publication of claim 1 characterized by performing said postinjection when said charge pressure or an inhalation air content is detected and this detection value is less than a predetermined value - claim 4.

[Claim 6] The charge pressure control unit of the internal combustion engine according to claim 5 characterized by setting up many postinjection quantity, so that said charge pressure or an inhalation air content is low to desired value.

[Claim 7] When an excess air factor is controlled at least using one side of the EGR control which makes a part of exhaust air flow back to inhalation of air, and the throttling control of an inhalation-of-air path and said exhaust air purification means has not carried out activity It is the charge pressure control unit of the internal combustion engine of any one publication of claim 3 characterized by controlling an excess air factor highly, so that there is much postinjection quantity while an excess air factor is controlled low and the exhaust air purification means is carrying out said postinjection after activity - claim 6.

[Claim 8] It is the charge pressure control unit of the internal combustion engine of any one publication of claim 3 characterized by carrying out postinjection while making small the bypass flow rate of said exhaust air even if it is the case where said exhaust air purification means has not carried out activity when there is an acceleration demand based on accelerator actuation of an operator and said charge pressure or an inhalation air content is less than a predetermined value - claim 7.

[Claim 9] The charge pressure control unit of the internal combustion engine according to claim 8 characterized by the time when an acceleration demand is larger making small the bypass flow rate of said exhaust air.

[Claim 10] The charge pressure control unit of the internal combustion engine according to claim 8 or 9 with which the time when an acceleration demand is larger is characterized by setting up said predetermined value greatly.

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#### DETAILED DESCRIPTION

[Detailed Description of the Invention]

(1000)

[Field of the Invention] This invention relates to charge pressure control of the internal combustion engine which carried the turbosupercharger.

[0002]

[Description of the Prior Art] By the diesel power plant for cars, wearing of exhaust air purification means, such as trap equipment which carries out uptake of the catalyst which is generally equipped with the supercharger for the improvement in an output, and purifies HC, CO, and NOx, or the PM (exhaust air particle), is beginning to be realized. When the exhaust air purification catalyst with which the turbine lower stream of a river of a turbosupercharger was equipped has not carried out activity to JP,5-44448,A, the exhaust air which bypassed the turbine and controlled cooling in a turbine is led to a catalyst, and the technique which was made to supercharge by stopping the bypass of said exhaust air is indicated after catalytic activity.

[Problem(s) to be Solved by the Invention] However, among an exhaust air bypass, when an acceleration demand is immediately after a catalyst carries out activity and stops an exhaust air bypass since the rotational speed of a supercharger is low (i.e., when the demand injection quantity increases), the response delay (rise delay of charge pressure) of a supercharger is large, and the increment in an inhalation air content does not catch up to the increment in fuel oil consumption, but an air-fuel ratio falls, and a possibility of inviting the increment in a smoke and aggravation of operability is.

[0004] This invention was made paying attention to such a conventional technical problem, controls the rise delay of charge pressure, and aims at enabling it to also maintain the exhaust air purification engine performance good.

MANA TITLE TO THE

[Means for Solving the Problem] For this reason, invention concerning claim 1 is the charge pressure control device of the internal combustion engine which carried the turbosupercharger which performs inhalation-of-air supercharge by the compressor which rotates with the turbine driven by the exhaust stream, and when raising the charge pressure of said turbosupercharger, it is characterized by performing postinjection after the Maine injection of a fuel.

[0006] Since according to invention concerning claim 1 an exhaust-gas temperature can be raised enough [ often / a response / and ] to an elevated temperature and the enthalpy of exhaust air of a turbine inlet port can be promptly increased by postinjection, turbine rotation can go up quickly and can raise charge pressure promptly by the compressor which this turbine and really rotates. [0007] Since the quantity of an inhalation air content is increased with a sufficient response when the time of the acceleration which increases a fuel, and charge pressure fall to below predetermined by this, the increment in a smoke can be prevented and good operability can be obtained. Moreover, invention concerning claim 2 is characterized by performing said Maine injection and postinjection with the injector [ ON-OFF / with a solenoid valve / injection of a fuel ].

[0008] According to invention concerning claim 2, the Maine injection and postinjection are controllable by ON-OFF of the fuel injection by the solenoid valve with high precision. Moreover, invention concerning claim 3 judges the active state of an exhaust air purification means to purify the exhaust air component which is arranged in the flueway of the turbine lower stream of a river of said turbosupercharger, and flows. The bypass flow rate of the exhaust air which bypasses said turbine and is led to said exhaust air purification means when this exhaust air purification means has not carried out activity is enlarged. When said exhaust air purification means carries out activity, while performing bypass control of flow which makes said bypass flow rate small, when switching said bypass flow rate to smallness from size, it is characterized by performing said postinjection.

[0009] According to invention concerning claim 3, when the exhaust air purification means [an NOx trap catalyst, an oxidation catalyst, DPF (diesel particulate filter), etc.] has not carried out activity at low temperature, the activity of an exhaust air purification means is promoted by enlarging an exhaust air bypass flow rate by controlling cooling of exhaust air by the heat dissipation to a

turbine, and raising an exhaust-gas temperature.

[0010] And if an exhaust air purification means carries out activity, said bypass flow rate will be switched to smallness (0 is included) from size, and the charge pressure of said turbosupercharger will be raised. At this time, charge pressure can be promptly raised by performing said postinjection, preventing the increment in a smoke. Moreover, invention concerning claim 4 is characterized by controlling the opening of the exhaust air bypass valve infixed in the bypass path which bypasses said turbine, and controlling said bypass flow rate.

[0011] According to invention concerning claim 4, said bypass flow rate can be enlarged by making said bypass flow rate small by making opening of an exhaust air bypass valve into smallness, and making opening of an exhaust air bypass valve into size. In addition, when switching the opening of an exhaust air bypass valve to smallness from size and increasing a bypass flow rate, it carries out, but postinjection is continuously performed, also when the charge pressure immediately after making opening of an exhaust air bypass valve into smallness is in a still low condition. Or opening of an exhaust air bypass valve is performed for postinjection, before the switch to smallness from size, and charge pressure can already be raised at the time of switch termination.

[0012] Moreover, invention concerning claim 5 is characterized by performing said postinjection, when said charge pressure or an inhalation air content is detected and this detection value is less than a predetermined value. According to invention concerning claim 5, since only between until charge pressure or an inhalation air content reaches a predetermined value carries out postinjection, it can minimize the period which carries out postinjection to which fuel consumption gets worse, and can be compatible in the fuel consumption engine performance a smoked reduction and operation disposition top.

[0013] Moreover, invention concerning claim 6 is characterized by said charge pressure or an inhalation air content setting up many postinjection quantity, so that it is low to desired value. Improvement in smoked reduction and operability is attained controlling the

fuel consumption aggravation by postinjection to the minimum, since the quantity of the postinjection quantity can be gradually decreased if many postinjection quantity is set up in early stages of acceleration when the delay of charge pressure is big since according to invention concerning claim 6 many postinjection quantity is set up so that charge pressure or an inhalation air content is low to desired value, and charge pressure goes up.

[0014] Moreover, invention concerning claim 7 is characterized by to control an excess air factor low, when an excess air factor is controlled at least using one side of the EGR control which makes a part of exhaust air flow back to inhalation of air, and the throttling control of an inhalation-of-air path and said exhaust-air purification means has not carried out activity, and to control an excess air factor highly, so that there is much postinjection quantity while the exhaust-air purification means is carrying out said postinjection after activity.

[0015] According to invention concerning claim 7, when the exhaust air purification means has not carried out activity at low temperature, an exhaust-gas temperature is raised by not performing postinjection but controlling an excess air factor low, it combines with the temperature up effectiveness by the bypass of exhaust air, and the temperature up of the exhaust air purification means can be carried out promptly, and it can carry out activity. Moreover, when postinjection is under operation, HC at the time of postinjection and aggravation of CO can be controlled by controlling an excess air factor highly.

[0016] Moreover, invention concerning claim 8 is characterized by carrying out postinjection, while making small the bypass flow rate of said exhaust air even if it is the case where said exhaust air purification means has not carried out activity when there is an acceleration demand based on accelerator actuation of an operator and said charge pressure or an inhalation air content is less than a predetermined value.

[0017] when there is an acceleration demand based on accelerator actuation of an operator according to invention concerning claim 8, even if it is the case where the exhaust air purification means has not carried out activity -- an exhaust air bypass flow rate -- small -- carrying out (0 being contained) -- since postinjection is carried out until charge pressure or an inhalation air content reaches a predetermined value, priority can be given to an acceleration demand and it can fill.

[0018] Moreover, invention concerning claim 9 is characterized by the time when an acceleration demand is larger making small the bypass flow rate of said exhaust air. According to invention concerning claim 9, the acceleration nature which brought the rise of charge pressure forward because the time when an acceleration demand is larger makes small the bypass flow rate of said exhaust air, and balanced the demand can be obtained.

[0019] Moreover, as for invention concerning claim 10, the time when an acceleration demand is larger is characterized by setting up said predetermined value greatly. According to invention concerning claim 10, by prolonging the period which carries out postinjection, the rise of charge pressure can be maintained and the acceleration nature corresponding to a demand can be obtained because the time when an acceleration demand is larger sets up said predetermined value greatly.

[0020]

[Embodiment of the Invention] Below, the operation gestalt of this invention is explained based on drawing. In drawing 1, the common rail type fuel-injection system which consists of a common rail 2, an injector [ON-OFF / with a solenoid valve / injector / injection of a fuel ] 3, and a supply pump which is not illustrated is used for the fuel-injection system of an engine (internal combustion engines, such as a diesel power plant) 1.

[0021] turbine 5T of a turbosupercharger 5 prepare in the lower stream of a river of an exhaust manifold 4 — having — this — it is equipped with compressor 5C on turbine 5T and the same axle. After compression pressurization is carried out by compressor 5C, inhalation of air passes along the inhalation-of-air path 6, and is inhaled in the cylinder of an engine 1 through a collector 7. In order to extract inspired air volume in the middle of the inhalation-of-air path 6, the inhalation-of-air throttle valve 8 is attached. Moreover, the charge pressure sensor 9 which detects charge pressure (intake pressure) is attached in the collector 7.

[0022] Said exhaust manifold 4 and inhalation-of-air path 6 are opened for free passage by the EGR path 10, and the amount of EGR gas is controlled by opening of the EGR valve 11 infixed in said EGR path 10. The flueway 12 of turbine 5T lower stream of a river is equipped with the sensor 14 whenever [ catalyst temperature ], in order to be equipped with a catalyst (exhaust air purification means) 13 and to detect the temperature of this catalyst 13. The exhaust manifold 4 of \*\*\*\*\*\*\*\*\* and the flueway 12 of the downstream are opened for free passage by the bypass path 15, and the opening area of the bypass path 15 is controlled by the exhaust air bypass valve

[0023] Whenever [ catalyst temperature / which was detected by the sensor 14 whenever / engine rotation speed signal / which was detected by the rotational-speed sensor 31 /, accelerator opening signal / which was detected by the accelerator opening sensor 32 /, and catalyst temperature ], a signal and the charge pressure signal detected by the charge pressure sensor 9 are inputted into the engine control unit 17, and the actuation command signal to an injector 3, the inhalation-of-air throttle valve 8, the EGR valve 11, and the exhaust air bypass valve 16 is outputted to it based on each signal.

[0024] Next, control of this operation gestalt is explained according to the flow chart of drawing 2. At step 1, Tcat and charge pressure Boost are read from each above-mentioned sensor whenever [engine-speed Ne, accelerator opening Acc, and catalyst temperature]. At step 2, it judges whether Tcat is less than [predetermined value T0] whenever [catalyst temperature]. Let the predetermined value T0 be a value (for example, 200-degreeC) equivalent to the activation temperature (temperature from which the effectiveness which purifies an exhaust air component generally becomes 50%) of a catalyst here.

[0025] When Tcat is less than [ predetermined value T0 ] whenever [ catalyst temperature ], it progresses to step 3 and judges whether the accelerator opening Acc is less than [ predetermined value A0 ]. That is, the existence of an acceleration demand of an operator is judged. Here, rate-of-change deltaAcc of accelerator opening may judge by whether it is less than deltaA0 predetermined value. When the accelerator opening Acc is less than [ predetermined value A0 ] (i.e., when it is judged that there is no acceleration demand), control which progresses to henceforth [ step 4 ] and promotes warming up of a catalyst 13 is performed.

[0026] Opening of the exhaust air bypass valve 16 is considered as full open, and the by-pass rate of turbine 5T is made to increase at step 4. Thereby, the temperature fall of the exhaust air which can control heat dissipation of exhaust air and is led to a catalyst to turbine 5T is controlled. It is referred to as postinjection-quantity Qp=0 at step 5. Postinjection of long duration is forbidden at the time of catalyst warming up, and fuel consumption aggravation and exhaust air performance degradation are controlled.

[0027] In step 6, a target EGR rate is set up in the following procedures. First, based on an engine speed Ne and the accelerator opening Acc, radical Motome label EGR rate MEGR0 is set up from the table of drawing 4. Next, based on Tcat, it asks for the 1st correction factor alpha of an EGR rate whenever [ catalyst temperature ] from the table of drawing 4. The 1st correction factor alpha of an EGR rate is set as such a large value that Tcat is [ whenever / catalyst temperature ] low like illustration. The product of radical Motome label EGR rate MEGR0 and the 1st correction factor alpha of an EGR rate is set to target EGR rate MEGR at the last. [0028] If an EGR rate is made to increase on condition that the same charge pressure, the air content inhaled to a cylinder will decrease and a rate with fuel oil consumption, i.e., an excess air factor, will fall. Since according to the above-mentioned actuation a target EGR rate is highly amended so that Tcat is [ whenever / catalyst temperature ] low, an excess air factor falls. Thus, by reducing

an excess air factor, the amount of air [ low temperature / under inhalation of air ] (new mind) decreases, and the inhalation-of-air temperature rise by increase in quantity of elevated temperature EGR gas can raise an exhaust-gas temperature conjointly, and can heighten the temperature up effectiveness of a catalyst.

[0029] When it is judged that Tcat carries out at step 2 and the catalyst is carrying out activity more than by predetermined value T0 whenever [ catalyst temperature ], or when the accelerator opening Acc is judged that there is an acceleration demand beyond predetermined value A0 at step 3, it progresses to step 7 so that priority may be given to supercharge and the acceleration engine performance may be secured, and opening of the exhaust air bypass valve 16 is made into a close by-pass bulb completely, and the bypass of turbine 5T is forbidden. In addition, when it progresses to step 7 from step 3, you may make it set up the opening of the exhaust air bypass valve 16 according to an acceleration demand. That is, it does not consider as a close by-pass bulb completely, but as the time when Acc-A0 (or delta Acc-delta A0) is larger is brought close to a close by-pass bulb completely, you may make it decrease the rate to bypass.

[0030] At step 8, it judges whether the detected charge pressure Boost is less than [ predetermined value B0 ], and in the case of below predetermined value B0, it is step 9, and it sets up the postinjection quantity Qp based on the map of drawing 5. Here, the postinjection quantity Qp is set as such a large value that charge pressure Boost is low. That is, by making [ many ] the postinjection quantity Qp and fully raising an exhaust-gas temperature, the enthalpy of a turbine inlet port can be enlarged, the exhaust air energy-recovery effectiveness in a turbine can be raised, the inhalation-of-air work of compression by the compressor can be made to be able to increase, and charge pressure can be promptly raised, so that charge pressure Boost is low. Here, when it has progressed from step 3, the predetermined value B0 may be set up according to a service condition (acceleration demand). That is, when Acc-A0 (or delta Acc-delta A0) is large, you may make it set up the predetermined value B0 greatly. Moreover, based on an inhalation air content, you may judge instead of charge pressure. Namely, it progresses to step 9 at the time of the inhalation air content Qac< desired value Qac0.

[0031] At the following step 10, a target EGR rate is set up with the following procedures. First, based on an engine speed Ne and the accelerator opening Acc, radical Motome label EGR rate MEGR0 is set up from the map of drawing 3 like step 6. Next, based on the postinjection quantity Qp, it asks for the 2nd correction factor beta of an EGR rate from the table of drawing 6. The 2nd correction factor beta of an EGR rate is set as such a small value that there is much postinjection quantity Qp like illustration. The product of radical Motome label EGR rate MEGR0 and the 2nd correction factor beta of an EGR rate is set to target EGR rate MEGR at the last. In order to make target EGR rate MEGR low by this so that there is much postinjection quantity Qp, an excess air factor will be set up highly. That is, the fuel postinjection was carried out [ the fuel ] by Excess EGR preventing carrying out a flame failure, a target EGR rate is set up so that the temperature up effectiveness by EGR can be acquired.

[0032] When charge pressure Boost is judged more than as predetermined value B0 at step 8, it progresses to step 11 and is referred to as postinjection-quantity Qp=0. Moreover, at the following step 12, based on an engine speed Ne and the accelerator opening Acc, radical Motome label EGR rate MEGR0 is read in the map of drawing 3, and this is set to target EGR rate MEGR. That is, reduction amendment of the target EGR rate by the postinjection quantity Qp is not performed. That is, postinjection enables it to maintain the sufficiently high temperature up effectiveness so that an exhaust-gas temperature may be made to shift to the temperature up by EGR after going up to some extent, a short-time deed and only when charge pressure is small since it leads to aggravation of fuel consumption, HC, and CO, although often [a response] and fully raised, and charge pressure may reach promptly to desired value. [0033] Finally, based on the target EGR rate set up at the above-mentioned steps 6, 10, and 12, the opening signal of the inhalation-of-air throttle valve 10 and the EGR valve 14 is calculated and outputted at step 13. In addition, although the case where only EGR control was performed was explained when controlling an excess air factor, the inhalation-of-air throttle valve 10 may be used together and controlled by the above-mentioned operation gestalt. That is, by carrying out throttling control of the inhalation-of-air throttle valve 10, and decreasing a direct air content, a response is good and an excess air factor can fully be made smaller than an EGR control independent case.

[0034] Moreover, although postinjection is performed with this operation gestalt after closing the exhaust air bypass valve 16, the initiation stage of postinjection may be set as a front [ stage / of the exhaust air bypass valve 16 / clausilium ], or coincidence.

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#### **DESCRIPTION OF DRAWINGS**

[Brief Description of the Drawings]

- [Drawing 1] Drawing showing the system configuration of the operation gestalt of this invention.
- [Drawing 2] The flow chart which shows the control routine of the above-mentioned operation gestalt.
- [Drawing 3] The map which searches for the radical Motome label EGR rate used with the above-mentioned operation gestalt.
- [Drawing 4] The map which similarly sets up the 1st correction factor alpha of an EGR rate.
  [Drawing 5] The table which similarly sets up the postinjection quantity Qp.
- [Drawing 6] The map which similarly sets up the 2nd correction factor beta of an EGR rate.
- [Description of Notations]
- 1 Engine
- 3 Injector
- 5 Turbosupercharger
- 5T Turbine
- 5C Compressor
- 8 Inhalation-of-Air Throttle Valve
- 9 Charge Pressure Sensor
- 10 EGR Path
- 11 EGR Valve
- 13 Catalyst
- 14 It is Sensor whenever [ Catalyst Temperature ].
- 15 Bypass Path
- 16 Exhaust Air Bypass Valve

## \* NOTICES \*

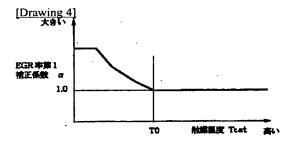
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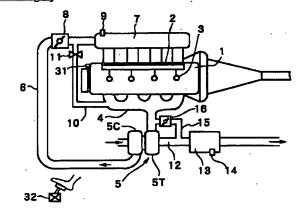
#### **DRAWINGS**

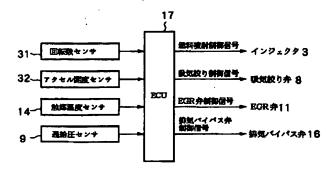
### [Drawing 3]



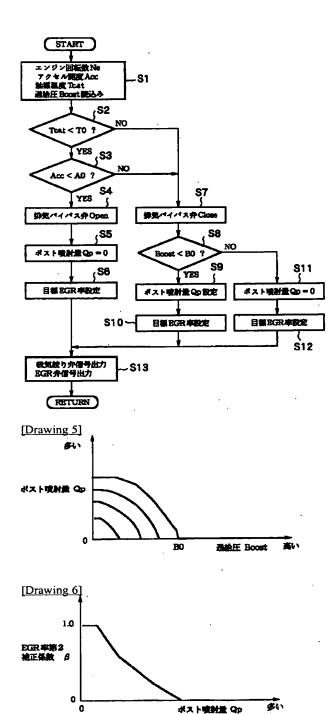


## [Drawing 1]





[Drawing 2]





### PATENT ABSTRACTS OF JAPAN

(11) Publication number: 2003120353 A

(43) Date of publication of application: 23.04.03

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(51) Int. Cl	F02D 23/00		
	F02B 37/00		
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	F02D 41/04		
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	F02D 43/00		
	F02M 25/07		
(21) Application	number: 2001315179	(71) Applicant:	NISSAN MOTOR CO LTD
(22) Date of filin	g: 12.10.01	(72) Inventor:	KAWAMOTO KEIJI

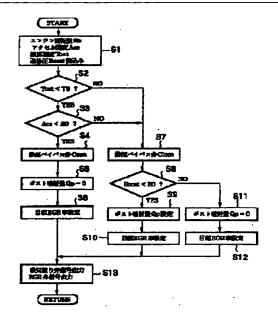
# (54) SUPERCHARGING PRESSURE CONTROL DEVICE FOR INTERNAL COMBUSTION ENGINE

#### (57) Abstract:

PROBLEM TO BE SOLVED: To improve the responsiveness of a supercharging pressure rise.

SOLUTION: If the temperature of an exhaust purifying catalyst is low and there is no acceleration request, exhaust bypassing a turbine of a turbosupercharger and maintaining high temperature is led to the catalyst to promote temperature raising activation (Step 1 to 4). In the process, if the catalyst is active or an acceleration request occurs, the exhaust bypassing of the turbine is prohibited, and if supercharging pressure is not higher than a given level, a postinjection is executed to elevate exhaust temperature and promote rises in turbine rotation and interlocked compressor rotation, which in turn suppresses lag in supercharging pressure rise. An excess air ratio corresponding to the postinjection quantity is controlled to suppress degradation in HC, CO and the like (Step 7 to 12).

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### (19)日本国特許庁(JP)

# (12) 公開特許公報(A)

(11)特許出願公開番号 特開2003-120353

(P2003-120353A)

(43)公開日 平成15年4月23日(2003.4.23)

(21)出願番号		特顧2001-315179(P26 平成13年10月12日(200					97 为事株式会社 県横浜市神奈川区宝町 2 番地		
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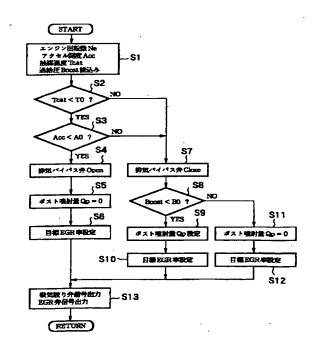
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## (54) 【発明の名称】 内燃機関の過給圧制御装置

#### (57)【要約】

【課題】 過給圧上昇の応答性を高める。

【解決手段】 排気浄化触媒の温度が低く、加速要求が 無いときにターボ過給機のタービンをバイバスさせて高 温に維持された排気を触媒に導いて昇温活性を促進し (ステップ1~4)、この状態から触媒が活性しあるい は加速要求が発生したときに、前記タービンの排気バイ パスを禁止し、かつ、過給圧が所定以下のときは、ポス ト噴射を行って排気温度を高め、タービン回転及び連動 するコンプレッサの回転上昇を早めて過給圧の上昇遅れ を抑制する。また、ポスト噴射量に応じた空気過剰率の 制御を行い、HC、CO等の悪化を抑制する(ステップ  $7 \sim 12)$ .



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#### 【特許請求の範囲】

【請求項1】排気流で駆動されるタービンと共に回転するコンプレッサにより吸気過給を行うターボ過給機を搭載した内燃機関の過給圧制御装置であって、前記ターボ過給機の過給圧を上昇させるとき、燃料のメイン噴射後のボスト噴射を行うことを特徴とする内燃機関の過給圧制御装置。

【請求項2】前記メイン噴射とポスト噴射とを、電磁弁により燃料の噴射をON-OFFするインジェクタにより行うことを特徴とする内燃機関の過給圧制御装置。

【請求項3】前記ターボ過給機のタービン下流の排気通路に配置されて流入する排気成分を浄化する排気浄化手段の活性状態を判断し、該排気浄化手段が活性していないときは前記タービンをバイパスして前記排気浄化手段に導く排気のバイパス流量を大きくし、前記排気浄化手段が活性したときは前記バイパス流量を小さくするバイパス流量制御を行うと共に、前記バイバス流量を大から小に切り換えるときに前記ボスト噴射を行うことを特徴とする請求項1または請求項2に記載の内燃機関の過給圧制御装置。

【請求項4】前記タービンをバイパスするバイパス通路 に介装された排気バイパス弁の開度を制御して、前記バイパス流量を制御することを特徴とする請求項3に記載 の内燃機関の過給圧制御装置。

【請求項5】前記過給圧あるいは吸入空気量を検出し、 該検出値が所定値を下回るとき、前記ポスト噴射を行う ことを特徴とする請求項1~請求項4のいずれか1つに 記載の内燃機関の過給圧制御装置。

【請求項6】前記過給圧あるいは吸入空気量が目標値に 対して低いほどポスト噴射量を多く設定することを特徴 30 とする請求項5に記載の内燃機関の過給圧制御装置。

【請求項7】排気の一部を吸気に還流させるEGR制御と、吸気通路の絞り制御との少なくとも一方を用いて空気過剰率を制御し、

前記排気浄化手段が活性していないときは、空気過剰率を低く制御し、排気浄化手段が活性後に前記ポスト噴射を実施しているときは、ポスト噴射量が多いほど空気過剰率を高く制御することを特徴とする請求項3~請求項6のいずれか1つに記載の内燃機関の過給圧制御装置。

【請求項8】運転者のアクセル操作に基づく加速要求がある場合は、前記排気浄化手段が活性していない場合であっても前記排気のバイバス流量を小さくするとともに、前記過給圧あるいは吸入空気量が所定値を下回る間は、ボスト噴射を実施することを特徴とする請求項3~請求項7のいずれか1つに記載の内燃機関の過給圧制御装置。

【請求項9】加速要求が大きいときほど前記排気のバイバス流量を小さくすることを特徴とする請求項8に記載の内燃機関の過給圧制御装置。

【請求項10】加速要求が大きいときほど前記所定値を

大きく設定することを特徴とする請求項8または請求項9に記載の内燃機関の過給圧制御装置。

【発明の詳細な説明】

[0001]

【発明の属する技術分野】本発明は、ターボ過給機を搭載した内燃機関の過給圧制御に関する。

[0002]

【従来の技術】車両用ディーゼルエンジンでは、一般に出力向上のため過給機を備えており、また、HC、CO、NOxを浄化する触媒やPM(排気微粒子)を捕集するトラップ装置などの排気浄化手段の装着が実現されはじめている。特開平5-44448号には、ターボ過給機のタービン下流に備えられた排気浄化触媒が活性していないときは、タービンをバイバスしてタービンによる冷却を抑制した排気を触媒に導き、触媒活性後は前記排気のバイバスを停止して過給を行うようにした技術が開示されている。

[0003]

【発明が解決しようとする課題】しかしながら、排気バイバス中は過給機の回転速度が低いため、触媒が活性して排気バイバスを中止した直後に加速要求がある場合、すなわち、要求噴射量が増加する場合、過給機の応答遅れ(過給圧の上昇遅れ)が大きく、燃料噴射量の増加に吸入空気量の増加が追いつかず、空燃比が低下し、スモークの増加や運転性の悪化を招くおそれがある。

【0004】本発明は、このような従来の課題に着目してなされたもので、過給圧の上昇遅れを抑制し、排気浄化性能も良好に維持できるようにすることを目的とする。

[0005]

【課題を解決するための手段】このため、請求項1に係る発明は、排気流で駆動されるタービンと共に回転するコンプレッサにより吸気過給を行うターボ過給機を搭載した内燃機関の過給圧制御装置であって、前記ターボ過給機の過給圧を上昇させるとき、燃料のメイン噴射後のポスト噴射を行うことを特徴とする。

【0006】請求項1に係る発明によると、ポスト噴射によって排気温度を応答良くかつ十分高温に高めて、タービン入口の排気のエンタルビを速やかに増大することができるので、タービン回転が急速に上昇し、該タービンと一体回転するコンプレッサによって過給圧を速やかに上昇させることができる。

【0007】これにより、燃料を増加する加速時や過給 圧が所定以下に低下したときなどに、吸入空気量が応答 良く増量されるので、スモークの増加を防止でき、良好 な運転性を得られる。また、請求項2に係る発明は、前 記メイン噴射とポスト噴射とを、電磁弁により燃料の噴 射をON-OFFするインジェクタにより行うことを特 敬とする。

【0008】請求項2に係る発明によると、電磁弁によ

る燃料噴射のON-OFFで、メイン噴射とポスト噴射 とを髙精度に制御することができる。また、請求項3に 係る発明は、前記ターボ過給機のタービン下流の排気通 路に配置されて流入する排気成分を浄化する排気浄化手 段の活性状態を判断し、該排気浄化手段が活性していな いときは前記タービンをバイパスして前記排気浄化手段 に導く排気のバイバス流量を大きくし、前記排気浄化手 段が活性したときは前記バイパス流量を小さくするバイ パス流量制御を行うと共に、前記バイパス流量を大から 小に切り換えるときに前記ポスト噴射を行うことを特徴 10

【0009】請求項3に係る発明によると、排気浄化手 段[NOxトラップ触媒、酸化触媒、DPF (ディーゼ ルパティキュレートフィルタ)など]が、低温で活性し ていないときは、排気バイパス流量を大きくすることに より、タービンへの放熱による排気の冷却を抑制して排 気温度を高めることにより、排気浄化手段の活性が促進 される。

【0010】そして、排気浄化手段が活性すると、前記 バイバス流量を大から小(0を含む)に切り換えて前記 ターボ過給機の過給圧を上昇させる。このとき、前記ボ スト噴射を行うことで、スモークの増加を防止しつつ速 やかに過給圧を上昇させることができる。また、請求項 4に係る発明は、前記タービンをバイパスするバイパス 通路に介装された排気バイパス弁の開度を制御して、前 記バイパス流量を制御することを特徴とする。

【0011】請求項4に係る発明によると、排気バイバ ス弁の開度を小とすることで前記バイバス流量を小さく し、排気バイパス弁の開度を大とすることで前記バイバ ス流量を大きくすることができる。なお、ポスト噴射 は、排気バイパス弁の開度を大から小に切り換えてバイ バス流量を増大するときに行うが、排気バイバス弁の開 度を小とした直後の過給圧がまだ低い状態のときも継続 して行う。あるいは、ポスト噴射を排気バイバス弁の開 度を大から小への切り換え前に行って、切り換え終了時 に既に過給圧が髙められているようにすることもでき

【0012】また、請求項5に係る発明は、前記過給圧 あるいは吸入空気量を検出し、該検出値が所定値を下回 るとき、前記ポスト噴射を行うことを特徴とする。請求 項5に係る発明によると、過給圧あるいは吸入空気量が 所定値に達するまでの間のみ、ポスト噴射を実施するの で、燃費が悪化するポスト噴射を実施する期間を必要最 小限にとどめられ、スモーク低減および運転性向上と、 燃費性能とを両立することができる。

【0013】また、請求項6に係る発明は、前記過給圧 あるいは吸入空気量が目標値に対して低いほどポスト噴 射量を多く設定することを特徴とする。請求項6に係る 発明によると、過給圧あるいは吸入空気量が目標値に対 して低いほどポスト噴射量を多く設定するので、加速初 50 モンレール2、電磁弁により燃料の噴射をON-OFF

期で過給圧の遅れが大きなときにはポスト噴射量を多く 設定し、過給圧が上昇してくると徐々にポスト噴射量を 減量できるので、ポスト噴射による燃費悪化を最小限に 抑制しつつ、スモーク低減と運転性の向上が可能とな

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【0014】また、請求項7に係る発明は、排気の一部 を吸気に還流させるEGR制御と、吸気通路の絞り制御 との少なくとも一方を用いて空気過剰率を制御し、前記 排気浄化手段が活性していないときは、空気過剰率を低 く制御し、排気浄化手段が活性後に前記ポスト噴射を実 施しているときは、ポスト噴射量が多いほど空気過剰率 を高く制御することを特徴とする。

【0015】請求項7に係る発明によると、排気浄化手 段が低温で活性していないときは、ポスト噴射を行わず 空気過剰率を低く制御することで排気温度を上昇させる ことができ、排気のバイバスによる昇温効果と併せて排 気浄化手段を速やかに昇温して活性することができる。 また、ボスト噴射を実施中のときは、空気過剰率を高く 制御することで、ポスト噴射時のHC、COの悪化を抑 制することができる。

【0016】また、請求項8に係る発明は、運転者のア クセル操作に基づく加速要求がある場合は、前記排気浄 化手段が活性していない場合であっても前記排気のバイ バス流量を小さくするとともに、前記過給圧あるいは吸 入空気量が所定値を下回る間は、ポスト噴射を実施する ことを特徴とする。

【0017】請求項8に係る発明によると、運転者のア クセル操作に基づく加速要求があるときは、排気浄化手 段が活性していない場合であっても、排気バイパス流量 30 を小さくする(0を含む)とともに、過給圧あるいは吸 入空気量が所定値に達するまでの間、ポスト噴射を実施 するので、加速要求を優先して満たすことができる。

【0018】また、請求項9に係る発明は、加速要求が 大きいときほど前記排気のバイパス流量を小さくするこ とを特徴とする。請求項9に係る発明によると、加速要 求が大きいときほど前記排気のバイバス流量を小さくす ることで過給圧の上昇を早めて要求に見合った加速性を 得ることができる。

【0019】また、請求項10に係る発明は、加速要求 が大きいときほど前記所定値を大きく設定することを特 徴とする。請求項10に係る発明によると、加速要求が 大きいときほど前記所定値を大きく設定することで、ポ スト噴射を実施する期間を引き伸ばすことにより過給圧 の上昇を維持し、要求に見合った加速性を得ることがで

[0020]

【発明の実施の形態】以下に、本発明の実施形態を図に 基づいて説明する。図1において、エンジン (ディーゼ ルエンジン等の内燃機関) 1の燃料噴射システムは、コ

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するインジェクタ3、及び、図示しないサプライボンプ から構成されるコモンレール式燃料噴射システムを採用 している。

【0021】排気マニホールド4の下流には、ターボ過 給機5のタービン5 Tが設けられ、該タービン5 Tと同 軸上にコンプレッサ5Cが装着されている。吸気はコン プレッサ5℃で圧縮加圧された後、吸気通路6を通り、 コレクタ7を介してエンジン1のシリンダ内に吸入され る。吸気通路6の途中には吸気量を絞るために吸気絞り 弁8が取り付けられている。また、コレクタ7には、過 給圧(吸気圧)を検出する過給圧センサ9が取り付けら れている。

【0022】前記排気マニホールド4と吸気通路6とは EGR通路10によって連通され、前記EGR通路10 に介装されたEGR 弁11の開度によってEGR ガス量 が制御される。タービン5 T下流の排気通路12には、 触媒 (排気浄化手段) 13が装着され、該触媒13の温 度を検出するため、触媒温度センサ14が装着されてい る。の上流側の排気マニホールド4と下流側の排気通路 12とは、バイパス通路15によって連通され、バイパ ス通路15の開口面積は排気バイパス弁16によって制 御される。

【0023】エンジンコントロールユニット17には、 回転速度センサ31で検出されたエンジン回転速度信 号、アクセル開度センサ32で検出されたアクセル開度 信号、触媒温度センサ14で検出された触媒温度信号、 および、過給圧センサ9で検出された過給圧信号が入力 され、各信号に基づいて、インジェクタ3、吸気絞り弁 8、EGR弁11、および、排気バイバス弁16への作 動指令信号を出力する。

【0024】次に、図2のフローチャートにしたがっ て、本実施形態の制御を説明する。ステップ1では、上 記各センサから、エンジン回転速度Ne、アクセル開度 Acc、触媒温度Tcat、過給圧Boostを読み込 む。ステップ2では、触媒温度Tcatが所定値TO未 満であるかを判定する。ここで所定値TOは、触媒の活 性化温度(一般的には、排気成分を浄化する効率が50 %となる温度)に相当する値(例えば、200°C)と する。

【0025】触媒温度Tcatが所定値T0未満である 場合、ステップ3へ進んで、アクセル開度Accが所定 値A O未満であるかを判定する。つまり、運転者の加速 要求の有無を判定する。ここで、アクセル開度の変化率 △Accが所定値△AO未満かどうかで判定してもよ い。アクセル開度Accが所定値AO未満の場合、つま り加速要求が無いと判断された場合は、ステップ4以降 へ進んで触媒13の暖機を促進する制御を行う。

【0026】ステップ4では、排気バイパス弁16の開 度を全開とし、タービン5Tのバイパス量を増加させ

き、触媒に導かれる排気の温度低下が抑制される。ステ ップ5では、ポスト噴射量Qp=0とする。触媒暖機時 には長時間のポスト噴射を禁止して燃費悪化、排気性能 の低下を抑制する。

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【0027】ステップ6では、以下の手順で目標EGR 率を設定する。まず、図4のテーブルからエンジン回転 速度Neとアクセル開度Accに基づき、基本目標EG R率MEGROを設定する。次に、図4のテーブルから 触媒温度Tcatに基づき、EGR率第1補正係数αを 求める。EGR率第1補正係数αは、図示のように触媒 温度Tcatが低いほど大きい値に設定されている。最 後に、基本目標EGR率MEGROとEGR率第1補正 係数αの積を目標EGR率MEGRとする。

【0028】同一過給圧の条件で、EGR率を増加させ ると、シリンダへ吸入する空気量が減少し、燃料噴射量 との割合、すなわち、空気過剰率が低下する。上記の動 作によると、触媒温度Tcatが低いほど目標EGR率 が高く補正されるため、空気過剰率は低下する。このよ うに、空気過剰率を低下させることにより、吸気中の低 温な空気(新気)の量が少なくなり、高温なEGRガス の増量による吸気温度上昇とも相まって排気温度を高め ることができ、触媒の昇温効果を高めることができる。 【0029】ステップ2で、触媒温度Tcatが所定値 T0以上で触媒が活性していると判断された場合、ある いは、ステップ3でアクセル開度Accが所定値A0以 上の加速要求があると判断された場合は、過給を優先し て加速性能を確保するようにステップ 7へ進み、排気バ イパス弁16の開度を全閉とし、タービン5下へのバイ パスを禁止する。なお、ステップ3からステップ7に進 30 んだ場合は、加速要求に応じて排気バイバス弁16の開 度を設定するようにしてもよい。すなわち、全閉とする のではなく、Acc−AO (あるいは△Acc−△A 0)が大きいときほど全閉に近づけるようにして、バイ

【0030】ステップ8では、検出した過給圧Boos t が所定値B0未満であるかを判定し、所定値B0未満 の場合は、ステップ9で、図5のマップに基づきポスト 噴射量Qpを設定する。ここで、ポスト噴射量Qpは、 過給圧Boostが低いほど大きい値に設定されてい 40 る。すなわち、過給圧Boostが低いほどポスト噴射 量Qpを多くして排気温度を十分に高めることにより、 タービン入□のエンタルピを大きくし、タービンによる 排気エネルギ回収効率を高め、コンプレッサによる吸気 圧縮仕事を増加させて、過給圧を速やかに上昇させるこ とができる。 ここで、ステップ3から進んできた場合 は、所定値B0は運転条件(加速要求)に応じて設定し てもよい。すなわち、Acc-AO(あるいは△Acc -△A0)が大きいときは所定値B0を大きく設定する ようにしてもよい。また、過給圧の代わりに、吸入空気 る。これにより、タービン5Tへの排気の放熱を抑制で 50 量に基づいて判定してもよい。すなわち、吸入空気量Q

パスする割合を減少させるようにしてもよい。

ac<目標値QacOのとき、ステップ9へ進む。

【0031】次のステップ10では、以下の手順により目標EGR率を設定する。まず、ステップ6と同様に図3のマップからエンジン回転速度Neとアクセル開度Accとに基づいて、基本目標EGR率MEGR0を設定する。次に、図6のテーブルからボスト噴射量Qpに基づいてEGR率第2補正係数βを求める。EGR率第2補正係数βは、図示のようにボスト噴射量Qpが多いほど、はでは、ま本目標EGR率MEGR0とEGR率第2補正係数βの積を目標EGR率MEGRとする。これにより、ポスト噴射量Qpが多いほど、目標EGR率MEGRを低くするため、空気過剰率を高く設定することになる。すなわち、過剰EGRによってボスト噴射された燃料が失火することを防止しつつEGRによる昇温効果を得られるように、目標EGR率を設定する。

【0032】ステップ8で過給圧Boostが所定値Bの以上と判定された場合は、ステップ11へ進み、ポスト噴射量Qp=0とする。また、次のステップ12で、図3のマップからエンジン回転速度Neとアクセル開度 20Accに基づいて、基本目標EGR率MEGR0を読み取り、これを目標EGR率MEGRとする。つまりポスト噴射量Qpによる目標EGR率の減少補正を行わない。すなわち、ポスト噴射は排気温度を応答良くかつ十分に高められるが、燃費やHC、COの悪化につながるため、過給圧が小さいときだけ短時間行い、ある程度上昇した後はEGRによる昇温に移行させて過給圧が目標値まで速やかに達するように十分高い昇温効果を維持できるようにする。

【0033】最後に、ステップ13で上記ステップ6、10、12で設定された目標EGR率に基づいて吸気絞り弁10およびEGR弁14の開度信号を演算し、出力する。なお、上記実施形態では、空気過剰率を制御する際にEGR制御のみ行う場合について説明したが、吸気\*

\* 絞り弁10を併用して制御してもよい。すなわち、吸気 絞り弁10を絞り制御して直接空気量を減少させること で、EGR制御単独の場合より応答良く、かつ、十分に 空気過剰率を小さくすることができる。

【0034】また、本実施形態では、排気バイバス弁16を閉じてからポスト噴射を行っているが、ポスト噴射の開始時期を排気バイバス弁16の閉弁時期より前、もしくは同時に設定してもよい。

【図面の簡単な説明】

10 【図1】本発明の実施形態のシステム構成を示す図。 【図2】上記実施形態の制御ルーチンを示すフローチャ

【図3】上記実施形態で用いる基本目標EGR率を求めるマップ。

【図4】同じくEGR率第1補正係数αを設定するマップ。

【図5】同じくポスト噴射量Qpを設定するテーブル。 【図6】同じくEGR率第2補正係数 $\beta$ を設定するマップ。

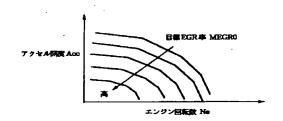
#### 【符号の説明】

- 1 エンジン
- 3 インジェクタ
- 5 ターボ過給機
- 5T タービン
- 5C コンプレッサ
- 8 吸気絞り弁
- 9 過給圧センサ
- 10 EGR通路
- 11 EGR弁
- 13 触媒

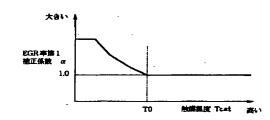
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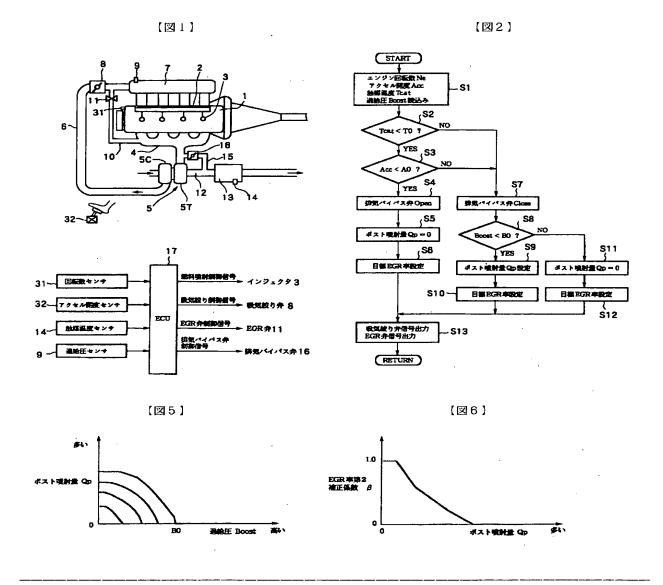
- 14 触媒温度センサ
- 15 バイパス通路
- 16 排気バイパス弁

[図3]



[図4]





フロントペー	ジの続き				
(51) Int .Cl .'		識別記号	FΙ		テーマコード(参考)
F 0 2 B	37/12	302	F 0 2 B	37/12	3 0 2 B
	37/18		F 0 2 D	21/08	301B
F 0 2 D	21/08	3 0 1			3 0 1 D
				23/02	F
	23/02			41/04	385B
	41/04	3 8 5		41/10	3 7 5
	41/10	3 7 5		43/00	301G
	43/00	3 0 1			3 0 1 N
					301R
					3 O 1 T

F O 2 M 25/07

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F 0 2 M 25/07 5 7 0

5 7 0 J 5 7 0 P

F 0 2 B 37/12

301A

Fターム(参考) 3G005 DA02 EA16 FA04 GB28 GD02

HA05 HA12 JA16 JA24 JA36

JA39 JA41 JA45 JB02

3G062 AA01 AA05 BA02 BA04 BA05

BA06 CA04 GA04 GA06 GA09

GA14 GA15 GA17 GA21

3G084 AA01 BA07 BA11 BA20 BA24

CA04 DA05 DA10 FA10 FA12

FA27

3G092 AA02 AA17 AA18 AB03 BA02

BA04 BB01 BB03 BB06 BB13

DB03 DC01 DC09 DC12 DC15

DE06S DF02 DF07 DF09

DG09 EA01 EA09 EA14 FA03

FA06 FA18 FA24 HA16X

HA16Z HB01X HB02X HD01X

HD02X HD02Z HD07X HD09X

HE01Z HF09Z

3G301 HA02 HA11 HA13 JA02 JA03

JA24 JA26 KA12 LA01 LB11

LC01 MA01 MA11 MA19 MA23

MA26 NE01 NE19 PA16Z

PB03Z PB05Z PD12Z PD15Z

PE01Z PF04Z